



***CBEg 6162- Advanced Chemical Engineering
Thermodynamics***

Postulates and equilibrium criteria

By

Dr. Eng. Shegaw Ahmed

School of Chemical & Bio Engineering

Addis Ababa Institute of Technology

Addis Ababa University

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CHAPTER-2-Postulates and equilibrium criteria

- *State of a Systems*
- *Fundamental Problems*
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- *Intensive parameters and Equations of State*
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Chapter 2. Postulates and equilibrium criteria

- The development of *classical thermodynamics* was largely based on the *heat engines and their performance*.
- In *the conventional treatments of classical thermodynamics*, the essential principles are presented through *four laws* of thermodynamics.
- The study of *classical thermodynamics* through *the postulation approach is a recent development* and it is gaining wide acceptance.
- It is found to be logically sound and provides *a better understanding* of the principles of thermodynamics *without depending upon the Carnot cycle*.



State of a system

- *Criteria for equilibrium* is necessary to characterize *the state of thermodynamic system*. The equilibrium state of a thermodynamic system can be described by specifying its *internal energy (U) volume (V) and the mole numbers* of the constituent species (N_1, N_2, \dots, N_c).



Fundamental problems in Thermodynamics

- In *thermodynamics analysis of processes* we are interested in determining the change in *the energy and other properties of the system* when it interacts with its surroundings or another system.
- Almost all problems in thermodynamics can be reduced to the following fundamental problem. If two given thermodynamic systems in their specified initial states are allowed to interact with each other:-
 - What will be *the resulting equilibrium state?* and
 - What are the *values of the extensive parameters* of the systems in that state?
 - The solution to the fundamental problem was *formulated through postulate.*



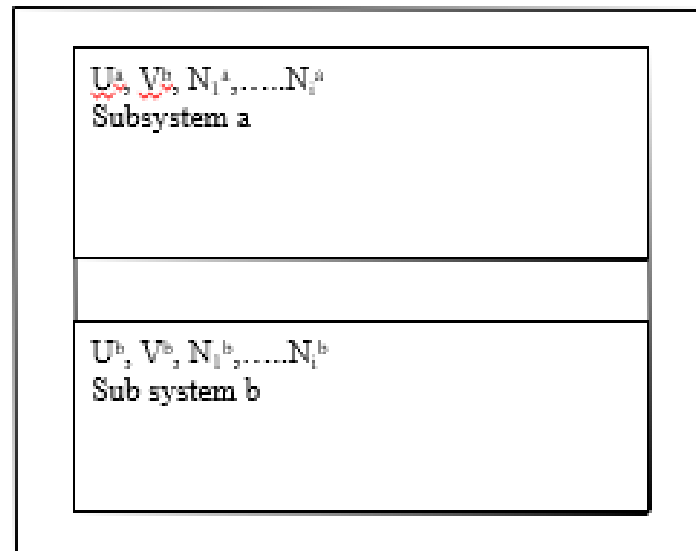
Fundamental problems in Thermodynamics

- Consider *an isolated composite system* consisting of two *subsystems a and b* which are separated from each other by *a rigid, adiabatic and impermeable boundary*.
- Let U_{0a} , V_{0a} , $N_{a1,0}, \dots, N_{ai,0}$ represent *the initial internal energy, volume, and constituent mole number* 1,2,3..i of system a.
- Similarly U_{0b} , V_{0b} , $N_{0b}, \dots, N_{i,0b}$ represent *the initial internal energy, volume and constituent mole* of system b.



Fundamental problems in Thermodynamics

- The *removal of each constraint initiates* a spontaneous process leading to *variation in the value of U, V, N, \dots, N_i* each subsystems.
- Then it requires to determine the *values of $U_a, V_b, N_{1a}, \dots, N_{ia}$ $U_b, V_b, N_{1b}, \dots, N_{ib}$ in the final equilibrium state.*





Postulates

- Solution to the fundamental problem in thermodynamics is formulated *through a set of postulates*,
- In the development of these postulates the central idea is *to find a simple formal solution to the fundamental problem.*
- The problem deals with *the determination of the final equilibrium state.*
- Some function of the independent variables, which are used to describe *the state of the system*, should reach an extremum value when the system attains **a state of equilibrium.**



Postulates -1-

- *This postulate states that the equilibrium-state of a thermodynamic-system is **completely characterized by extensive variables $U, V, N_1... N_c$. The entropy (S) of such a system** is a function of these variables and, in the **absence of internal constraints**, the variables assume such values as **to maximize the entropy** over all possible constrained equilibrium states.*
- *This postulate states that the equilibrium state of a thermodynamic system is **completely characterized by internal energy, volume, and the mole numbers** of the constituents of the system*



Postulates -2-

- The *entropy of the system increases monotonically with increasing internal energy* and is *equal to zero in the state where* $\left(\frac{\partial U}{\partial S}\right)_{vN_i} = 0$ The entropy is *additive and a continuous and differentiable function.*
- This postulate states that *the entropy of a system increases with increasing internal energy.* That is $\left(\frac{\partial S}{\partial U}\right)_{vN_i} > 0$
- It will be shown that the temperature is defined by the relation

$$\left(\frac{\partial S}{\partial U}\right)_{vN_i} = \frac{1}{T}$$



Example 1

- Consider an isolated composite system consisting of two subsystems a and b which are separated from each other by a rigid, adiabatic and impermeable boundary. The initial values of the extensive parameters in these subsystems are $U_a = 7.2 \text{ MJ}$, $V_a = 1 \text{ m}^3$, $N_a = 1 \text{ kmol}$, $U_b = 7.2 \text{ MJ}$; $V_b = 1 \text{ m}^3$, $N_b = 2 \text{ kmol}$. If the internal boundary is made diathermal, determine the final state of equilibrium. The fundamental relation $S = K(UVN)^{1/3}$ where S is in kJ/K ; N in kmol , V in m^3 and U in kJ and K is a constant with appropriate dimensions, is valid for both the subsystems.



Intensive Parameters and equation of states

- The relations which *express the intensive parameters as a function of the independent extensive parameters* are called *equation of state*.
- An equation of state is *a homogeneous zero order function* of the extensive parameters.
- The *fundamental relation in the entropy* representation is given by $S = S(U, V, N_1, N_2, \dots, N_c)$ and the *set $U, V, N_1, N_2, \dots, N_c$* are called *the extensive parameters in the entropy representation*. The intensive parameters and the equations of state in the entropy representation are given by



Entropy Representation

$$\left(\frac{\partial S}{\partial V}\right)_{U,V,N_1,\dots,N_c} \equiv \frac{P}{T} = \frac{P}{T}(U,V,N_1,N_2,\dots,N_c)$$

$$-\left(\frac{\partial S}{\partial N_i}\right)_{U,V,N_j} \equiv \frac{\mu_i}{T} = \frac{\mu_i}{T}(U,V,N_1,N_2,\dots,N_c)$$

The differential of S is given by

$$dS = \frac{1}{T}dU + \frac{P}{T}dV - \sum_{i=1}^c \frac{\mu_i}{T}dN_i$$



Energy Representation

The fundamental relation in the energy representation is given by

$$U = U(S, V, N_1, N_2 \dots N_c)$$

*and the set of variables $S, V, N_1, N_2 \dots N_c$ are called **the extensive parameters in the energy representation**. The intensive parameters and the equations of state in the energy representation are given by*

$$\left(\frac{\partial U}{\partial S} \right)_{V, N_1, \dots, N_c} \equiv T = T(S, V, N_1, N_2 \dots N_c)$$

$$\left(\frac{\partial U}{\partial V} \right)_{S, V, N_1, \dots, N_c} \equiv P = P(S, V, N_1, N_2 \dots N_c)$$

$$-\left(\frac{\partial U}{\partial N_i} \right)_{S, V, N_j} \equiv \mu_i = \mu_i(S, V, N_1, N_2 \dots N_c)$$

The differential of U is given by $dU = TdS - PdV + \sum_{i=1}^c \mu_i dN_i$



Example 2

The fundamental relation for a particular thermodynamic system is given by $U = CS^3/NV$ where C is a positive constant.

- a) Obtain the **three intensive parameters T , P and μ** and write the **three equations of state** of the system
- b) Show that the three equations of state are **homogenous functions of zeroth order**
- c) Express **μ as a function of T and P**



Criteria of Equilibrium

- For the system to be in *a state of thermodynamic equilibrium* it should simultaneously satisfies *the criteria of thermal, mechanical and chemical equilibrium*.
- Consider *an isolated composite system*, consisting of two subsystems a and b, the sub-system are separated from each other by *a rigid adiabatic and impermeable boundary*. The subsystem a is characterized by U^a , V^a , N^a and the subsystem b is characterized by U^b , V^b , N^b .



Thermal Equilibrium

- If the internal boundary is made *diathermal*, *energy flow in the form of heat between the two subsystems* till a state of thermal equilibrium is established.
- Since the internal boundary is *rigid, diathermal and impermeable*, it is *restricted* with respect to *volume and mole numbers of the constitute species* but allows the *exchange of energy* in the form of heat.



Thermal Equilibrium

- However, the composite system is *isolated* and hence *the total energy of the composite system remains constant*.
- In state of *thermal equilibrium*, *the temperature of subsystem a* must be identical to *the temperature of subsystem b*. Hence *the criteria for thermal equilibrium* is given by

$$\frac{1}{T^a} = \frac{1}{T^b}$$



Example 3

- Consider an isolated composite system consisting of two subsystems a and b which are separated from each other by a rigid, adiabatic and impermeable boundary. The extensive parameters of the subsystems are $U_a = 7.2 \text{ MJ}$, $V_a = 1 \text{ m}^3$, $N_a = 1 \text{ kmol}$, $U_b = 7.2 \text{ MJ}$; $V_b = 1 \text{ m}^3$, $N_b = 2 \text{ kmol}$. The fundamental relation $S = K(UVN)^{1/3}$ where S is in kJ/K ; N in kmol , V in m^3 and U in kJ and K is a constant with appropriate dimensions, is valid for both the subsystems. If the internal boundary is made diathermal, determine the final equilibrium values of U_a , U_b and temperature. Assume $K = 6 \times 10^5$.



Mechanical Equilibrium

- If the internal boundary is made *movable and diathermal* the composite system eventually settles into *a new state of equilibrium*. The internal boundary *allows the exchange of volume* and *energy between the two subsystems*.
- However, *the total volume and energy of the composite system remains constant*.
- *In state of mechanical equilibrium, the pressure of subsystem a must be identical to the pressure of subsystem b*. Hence the criteria for mechanical equilibrium is given by
$$\frac{P^a}{T^a} = \frac{P^b}{T^b}$$



Example 4

- Consider *an isolated composite system consisting of two subsystems a and b* which are separated from each other by *a rigid, adiabatic and impermeable boundary*. The extensive parameters of the subsystems are $U_a = 7.2 \text{ MJ}$, $V_a = 1 \text{ m}^3$, $N_a = 1 \text{ kmol}$, $U_b = 7.2 \text{ MJ}$; $V_b = 1 \text{ m}^3$, $N_b = 2 \text{ kmol}$. The fundamental relation given below with $R = 8.314 \text{ kJ/kmol K}$ is valid for both the systems.

$$S = (N/N_o) * S_o + NR \ln [(U/U_o)^{3/2} V/V_o (N/N_o)^{-5/2}]$$

$$\text{Where } S_o = 5/2 N_o R - N_o (\mu/T)_o.$$

U_o , V_o , N_o , $(\mu/T)_o$ refer to the parameters of a fictitious state

If the internal boundary is made *diathermal and movable*, *determine the final equilibrium values of U_a , V_a , U_b , V_b , temperature and pressure.*



Chemical Equilibrium

- If the internal boundary is made *diathermal and semi-permeable* which permit *the transfer of constituent 1 only and does not allow the transfer of other constitute*, the composite system settles in to a new state of equilibrium.
- Since the internal boundary is *diathermal and semi-permeable*, it allows *the exchange of internal energy and the mole number of constitute 1 only between the two sub systems*, but *does not allow* the transfer of other constitutes through it.



Chemical Equilibrium

- Moreover as the composite system is *isolated the total energy and the total mole numbers of constitute 1 should be constant.*
- *In state of chemical equilibrium, the chemical potential of subsystem a* must be identical to *the chemical potential of subsystem b*. Hence the criteria for chemical equilibrium is given by

$$\frac{\mu_i^a}{T^a} = \frac{\mu_i^b}{T^b}$$



Example 5

- An isolated composite system consisting of two subsystems a and b. Initially the subsystems are separated from each other by a rigid, adiabatic and impermeable boundary. If the internal boundary is made diathermal and semipermeable which allows the transfer of constituent 1 only, determine the values of U_a , U_b , N_{1a} , N_{1b} and T in the final state of equilibrium. Assume that both the subsystems a and b obey the fundamental relation for a binary mixture given by*

$$S = (N_1+N_2)R \ln [U^{3/2}V(N_1+N_2)^{-5/2}] - N_1R \ln N_1/(N_1+N_2) - N_2R \ln N_2/(N_1+N_2) + (N_1+N_2)CK(UV/N)^{1/3}$$

- where $R = 8.314 \text{ kJ/kmol K}$ and C is an unknown constant. The subscripts 1 and 2 denote the constituents.*